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Characterizing Sediment Physical Property Variability for Bench Scale Dewatering Purposes

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Abstract

A field sampling program was undertaken to assess the variability of physical characteristics of contaminated sediments in a large (160 ha) effluent stabilization lagoon. The objective of this paper is to use this “field lab” as a basis for comparing different sampling techniques (i.e. discrete and composite) for remediation-based evaluations (i.e. sediment volume estimates and bench scale dewatering studies). The distribution of sediment thickness measured throughout the lagoon by gravity core sampling is presented for context. Selected gravity core sediment samples are evaluated with respect to physical property (water/solids content, bulk density, and particle size) variability in both the vertical (i.e. within a single gravity core) and spatial directions (among gravity cores). Composite samples created via homogenization of a single entire gravity core is performed to compare to the discrete and average physical properties of a nearby gravity core. Vacuum-based samples are also compared to gravity core samples in terms of particle size. It is demonstrated that by understanding sediment variability, composite samples can be shown to be an efficient method of obtaining representative samples. When large samples for dewatering trials are required, vacuum sampling can produce samples with similar mean particles size to discrete and composite samples.

Keywords chosen from ICE Publishing List

Contaminated material; Geotechnical engineering; Waste management & disposal

List of notations

None

1 **Introduction**

2 The Boat Harbour Stabilization Lagoon (BHSL) is part of an industrial wastewater treatment facility (160 ha
3 in plan area, Tackley, 2019) located in Pictou County, Nova Scotia, Canada. This lagoon was originally a
4 tidal estuary until it was separated from the Atlantic Ocean (i.e. Northumberland Strait) via modifications
5 introduced by the provincial government in 1967 (Hoffman et al., 2019). These modifications were
6 completed in order to transition the estuary into a wastewater treatment facility for predominately pulp and
7 paper process effluent, although other industrial operations are also known to have contributed to the
8 wastewater effluent since 1967 (Hoffman et al., 2019). During operation, up to 75,000 m³ of wastewater
9 was discharged to the treatment facility daily (GHD, 2018). Over 50 years of operation have resulted in the
10 accumulation of a thin layer of organic-rich, black sediment in the BHSL (GHD, 2018). This black sediment,
11 which is underlain by a native grey marine sediment, contains a mix of inorganic and organic contaminants
12 (i.e. metal[loid]s, polycyclic aromatic hydrocarbons [PAHs], dioxins and furans) present above regulatory
13 limits (Hoffman et al., 2017; Hoffman et al., 2019). BHSL has been effectively closed since January 2020;
14 remediation to its pre-industrial state is underway (i.e. a tidally influenced estuary). It is anticipated that
15 dredging of the BHSL will result in the dewatering of greater than 577,000 m³ of unconsolidated sediment
16 followed by storage in a secure containment cell (GHD, 2018). This site serves as an opportunity to
17 compare different sediment sampling methodologies for remediation purposes, such as those explored in
18 this paper.

19
20 Given that sediment properties are site and location specific, it is critical before establishing a
21 dewatering/remediation approach that effective sampling protocols be developed to ensure representative
22 samples are obtained. This is true for bench scale dewatering trials as well as estimating required volumes
23 for future sediment containment structures. Sediment characteristics such as solids content, particle size
24 distribution, and density must be established to prepare a basis for an effective sediment management plan
25 (Reis et al., 2007). Past studies have also identified the need for assessing sediment properties prior to
26 remediation efforts (e.g. Mao, 1997; Ya, 2017) as physical and chemical properties of sediment deposits in
27 aquatic ecosystems may vary spatially (Reis et al., 2007).

28

29 Understanding the variability in sediment composition is particularly important when considering bench
30 scale dewatering studies and sediment volume estimations, as these studies often require the use of large
31 sample volumes from a given depth and location to represent the contaminated sediment throughout a
32 large sampling area. The BHSL is an excellent “field lab” to assess how different sampling methods
33 influence the determination of sediment physical characteristics; the large areal extent and potentially highly
34 variable characteristics with depth at BHSL are typical of other contaminated waste ponds. The objectives
35 of this paper are: 1) to present a method of comparing time-consuming discrete sampling techniques to
36 more time-efficient composite sample techniques. This is particularly relevant for volume estimates of
37 contaminated sediments, and, 2) to present a method of comparing composite sampling techniques to a
38 vacuum sampling technique developed for this project. The vacuum sampling method produces large
39 volumes of sediment for bench scale dewatering purposes but involves significant physical disturbance of
40 the sample. To investigate these objectives, the distribution of sediment thickness measured throughout the
41 lagoon by gravity core sampling is presented; extrusion of these gravity core samples are then performed to
42 evaluate sediment physical properties in both the vertical (i.e. within a single gravity core) and spatial
43 directions (between gravity cores) and provide context for the sediment’s variability. Composite samples
44 are created by homogenization of single entire gravity cores to compare to the discrete subsamples and
45 average discrete subsample physical properties (i.e. water/solids content, bulk density, and particle size) of
46 a nearby gravity core and also provide some comparison to vacuum samples. Vacuum-based samples are
47 compared to gravity core samples (both discrete and composite) in terms of particle size (i.e. a key physical
48 parameter for dewatering).

49

50 **2. Experimental Work**

51 **2.1 Sediment sampling**

52 Figure 1 shows sampling locations (i.e. gravity core and vacuum samples) throughout the BHSL, taken over
53 a four-year period (i.e. 2016-2019). Area A was isolated from the remainder of the BHSL in March 2017 by
54 an earthen berm (shown in Figure 1) for pilot dewatering studies (GHD, 2018). The rest of the lagoon,
55 which was receiving effluent at the time of sampling, has been subdivided into three regions (Area B, C,
56 and D) in this study to assess the variability of sediment characteristics throughout the BHSL.

57

58 The majority of samples (151 cores in total) were obtained using a gravity corer (60 cm in length and
59 6.5 cm in diameter) (Glew et al., 2001). The device was ideal for this site, as much of the contaminated
60 sediment was shallower than the core length. This coring method has been shown to be reliable for taking
61 core samples sufficient for precise paleolimnology work (Dunnington et al., 2017). The device consisted of
62 a collar, which secured the core barrel, and a spring release mechanism. The weight of the device, when
63 secured to the core barrel, allowed it to easily penetrate the sediment (see Figure S1). During the core
64 penetration, the top of the core barrel remained open until a weighted messenger was lowered to trigger the
65 device. At this time, the spring mechanism was activated, and suction was maintained in the core barrel
66 with a rubber stopper until the sample was brought to the surface. Upon recovery, the sample was then
67 sealed at each end for transport. The method is simple, inexpensive, and does not require supplementary
68 mechanical assistance (i.e. a winch).

69

70 151 cores were used for thickness determination to assess variability throughout BSHL. A spatial analysis
71 of the thickness distribution in the BSHL was conducted using the ArcGIS (10.5) “Topo to Raster”
72 interpolation method for “lake polygons”. This method is specifically designed to analyze contour and
73 elevation inputs (Esri, 2019) and can be constrained to the limit of a given polygon (BSHL in this case). The
74 interpolation used a 1 m x 1 m cell length (resolution), with contour lines representing each 5 cm change in
75 thickness. The map presents a realistic interpretation of the sediment thickness, based on the data which
76 was available at the time of publication (additional data points may alter this interpolation). This information
77 is presented to provide an indication of the distribution of sediment throughout the BSHL.

78

79 In addition, 30 of the 151 sediment cores were selected for detailed physical testing (i.e. beyond sediment
80 thickness determination) and were transported to Dalhousie University laboratories for analysis. Nineteen
81 (19) of these cores were used to obtain vertically discrete samples (described in detail below), and the
82 remaining 11 were used for depth integrated composite samples. Variability in physical properties (i.e.
83 particle size, water / solids content) at different depths (vertically) were investigated using discrete vertical
84 samples. Sample 19-01 was selected for discrete particle size analyses. To obtain these discrete samples,

85 sediment in the core was sampled at 5cm intervals using an extruder (Glew et al., 2001). As can be seen in
86 Figure S2, the extruder apparatus consisted of an aluminum rod (shaft) connected to a base and situated
87 vertically. An extruding disk that was slightly smaller than the core barrel diameter was placed at the top of
88 the rod. A core holder (collar) was situated below the extruding disk, which allowed for an accurate and
89 controlled descent of the core barrel. After carefully removing the rubber stopper at the bottom of core
90 barrel, the core barrel was mounted on top of the extruding disk. The top rubber stopper was then removed
91 from the core barrel and a sampling stage was attached to the top of the barrel. The core barrel was moved
92 downward to remove the top water until the top of the sediment was even with the sampling stage. A series
93 of spacer plates (5cm aluminum cuboids) were placed on the adjuster disc, which was situated on the shaft,
94 below the collar. The adjuster disc was carefully moved upward until the top of the aluminum cubes
95 touched the bottom of the core holder, then was secured in place. At this time, one of the aluminum cuboids
96 was removed, and the core barrel gently pulled downward to extrude 5 cm of sediment from the barrel.
97 Each extruded sample was then removed from the sampling stage into pre-labeled sample bags (showing
98 core ID, depth and date), weighed, and refrigerated at 4°C until further analysis. Although each increment
99 was 5 cm, smaller increments were used to section the 5 cm increment near the black / grey sediment
100 interface. After weighing each 5 cm sediment interval, the center portion of each interval was isolated for
101 further analysis, while the surrounding sediment was trimmed and discarded to avoid portions which may
102 have been smeared due to the sampling tube penetration.

103
104 In addition to discrete samples, 11 individual cores were homogenized to create a composite sample that
105 simulates the mixing of the sediment that will occur during a dredging process. Composite samples were
106 also used to compare to sediment properties at each discrete sampling location (spatially) throughout the
107 BHSL. For each composite sample, the total thickness of sediment in one core was mixed, weighed, and
108 then stored in sterile containers at 4°C. At the time of analysis of the composite specimens, sediments in
109 the container were mixed thoroughly, homogenized, and a representative sample from each composite
110 sample was selected for water / solids content, density and particle size analyses. All 11 composite
111 samples were then evaluated for mean and variation range values of each of these physical properties.

112

113 A vacuum sampling method was used to simulate sediment sampling conditions which could arise during a
114 dredging procedure. A barge of 4.5 m × 2 m was constructed from high density polyethylene (HDPE) pipe
115 (sealed) to form the support for the wooden platform decking. The barge and sampling gear were then
116 towed by a boat to the desired sampling location. Anchors were used to fix barge in position while sampling
117 was performed. A gas-powered generator was used to power an electric submersible vacuum pump (560-
118 watt stainless steel sewage pump), which in turn was used to recover the sediment. The pump was hand-
119 lowered into the water, to the surface of the sediment, via a rope secured to the pump. Upon engagement
120 of the pump, the sediment was drawn through a 50 mm diameter tube, 3 m in length, to the surface of the
121 barge and placed in a 20L container (see Figure S3). The pump was situated at various locations on the
122 basin bottom in order to obtain eight 20 L containers of the sediment, which were then transported to
123 Dalhousie University in Halifax, Canada for characterization tests. Vacuum sampling results in a
124 significantly disturbed sample with added water being entrained in the vacuum process.

125

126 **2.2 Physical analysis**

127 Physical characteristics of the black sediment were evaluated at Dalhousie University laboratories. The
128 water / solids content (relevant ASTM standard D2216, last revised 2019), bulk density, specific gravity
129 (ASTM D854, 2014), organic material (ASTM D2974, 2020), and particle size were measured for selected
130 samples (i.e. discrete and composite cores). Each measurement was repeated three times for all
131 experiments. Water / solids content and density measurements are important for remediation projects
132 utilizing containment approaches for volume estimates of remediation projects while particle size analyses
133 are useful when developing dewatering approaches. Specific gravity and organic carbon determinations
134 were used for characterization purposes only.

135

136 Particle size distributions of the sediment were evaluated using a micro flow imaging technique (MFI-
137 DPA4100/4200-Series B) (Mackie, 2010), which counts particle sizes from 2 to 400 µm. In this technique, 1
138 ml of sample fluid (1% dilution by volume was used for all of the samples in this study) was captured in
139 successive image frames as the sample stream passed through a flow cell. Frame images displayed during
140 operation provided immediate visual feedback on the nature of the particle population in the sample.

141 Images were also digitally analyzed using the software to compile a database containing count, size, and
142 concentration, and to produce parameter distributions using histograms and scatter plots (Sharma et al.,
143 2010).

144

145 **2.3 Statistical analysis**

146 A statistical analysis was performed for the physical test data collected. The mean physical properties
147 obtained for discrete, composite, vacuum samples as well as area groupings were compared using Tukey's
148 comparison test of one-way analysis of variance (ANOVA) in Minitab. ANOVA is used to determine whether
149 the mean of two or more groups differ, and Tukey's method is used to formally test whether the difference
150 between a pair of groups is statistically significant. Tukey's method also provides a range of values showing
151 the confidence interval for the difference between the means for each pair of groups. If this range does not
152 include zero, it means that the difference between these means is significant (Minitab express support,
153 2019).

154

155 **3. Results and Discussion**

156 As previously mentioned, the black sediment layer in the BHSL consisted mostly of solids accumulated
157 from predominantly pulp and paper treated wastewater since the 1960s. Results from organic material
158 testing showed the solid portion of black sediment contained 25% - 31% organic carbon with a specific
159 gravity of 1.71 (± 0.13 SD).

160

161 For context of the distribution of sediment thickness throughout the BHSL, Figure 2 presents the frequency
162 distribution of black sediment thicknesses measured in the 151 gravity core samples. For example, a 35 cm
163 thickness of black sediment was measured in 16 samples." An average thickness of 26.6 cm (± 12.2 SD)
164 was measured in black sediment. The maximum thickness of approximately 45 cm for the black sediment
165 was identified in core samples of BH 17-34, BH 17-33, and BH 19-82-100.

166

167 A contour map of the spatial distribution of sediment thickness determined using the methods previously
168 described is presented in Figure 3. The results show the black sediment was not evenly distributed across

169 the BHSL; sediment thickness is greatest in Area B (west side of BHSL, near the location of cores BH 17-
170 34 and BH 17-33). A bathymetric survey indicates that this location is the deepest part of the basin
171 (Spooner and Dunnington 2016). The thicker sediment in this location is likely due to its proximity to the
172 effluent inflow point (Figure 3), and with increasing distance from that point (notably in Areas C and D), the
173 thickness decreases.

174
175 To examine the influence of this varying distribution of sediment on its physical properties, Figure 4 shows
176 both water and solids content, versus depth for the 19 discrete gravity core samples. Results are plotted
177 relative to distance from the black / grey interface (dotted line). Due the large amount of data (shown in
178 Figure 4S), data has been presented in term of mean and one standard deviation from the mean for each
179 depth. The focus of this study was the black sediment characterization, however, grey sediment properties
180 (water / solids content) were also evaluated in selected cores and are shown for reference. Results show
181 that discrete samples, regardless of location, show a similar water / solids content trend. As expected,
182 water content decreased with depth (Figure 4(a)), as self-weight consolidation of settled particles occurred.
183 In this study, the black sediment exhibited high water contents (max 3200%) near the surface (0-5 cm)
184 which decreased to around 500% at the black / grey sediment interface.

185
186 Water /solid content and density are key parameters to understand for remediation projects involving
187 containment cells of dredged sediments. The self-weight consolidation process also resulted in the solids
188 content increasing with depth from an average of 2% at the water / black sediment interface to around 12%
189 at the black / grey sediment interface (Figure 4(b)). Likewise, the density of the black sediment increased
190 with depth, increasing from 1.01 g/cm³ near the surface (0-5cm) to 1.17 g/cm³ at 45 cm below the black
191 sediment-water contact (as presented in Table 1 and Figure S5). The density of composite samples,
192 however, was 1.07 g/cm³, which was close to the average density of discrete samples (1.10 g/cm³).

193

194

195

196

Table 1. Density values of discrete and composite samples.

Depth (cm)	Density (g/cm ³) Mean + SD
0-5	1.01 ± 0.13
5-10	1.06 ± 0.03
10-15	1.08 ± 0.04
15-20	1.07 ± 0.04
20-25	1.18 ± 0.21
25-30	1.13 ± 0.08
30-35	1.10 ± 0.02
35-40	1.11 ± 0.02
40-45	1.17 ± 0.07
Average of discrete samples	1.10 ± 0.05
Composite samples	1.07 ± 0.05

197

198 Box-whisker plots (Figure 5(a) & 5(b)) present the range of water / solids content of black sediments for the
199 cores used to create discrete and composite samples, as well as samples taken using the vacuum pump.
200 For individual discrete samples, the plot represents data taken vertically in the core, while for composite
201 samples, the plot represents the data analysis of a combination of all composite samples. For comparison,
202 the data analysis of all discrete samples for each of the four areas (A, B, C, and D) are also shown. The
203 box-whisker plot is a standard technique for presenting a 5-number summary of a dataset which consists of
204 the minimum and maximum range values, the upper and lower quartiles, and the median (the line that
205 divides the box into two parts). In the box plot, an outlier is an observation that is numerically distant from
206 the rest of the data and is defined as a data point that is located outside the whiskers of the box plot. This
207 collection of values is an effective way to summarize the distribution of a dataset (Williamson et al., 1989).
208 In Figure 5, boxes with the same pattern show the cores taken from the same area, while grey colored
209 boxes represent the data analysis for the collection of discrete samples from the given area. The solid black
210 boxes represent the vacuum samples taken from Area A and B, and the solid white box shows the dataset
211 of composite samples.

212

213 One-way ANOVA test results (using the Tukey method with 95% confidence) indicated that there was no
214 significant difference between water / solids content of different cores representing discrete samples
215 throughout the BHSL. In this study, Tukey's results are shown with the letters on the graphs. In Figure 5,
216 samples attributed with identical letters are not significantly different.

217

218 As presented in Figure 5, an average water content and solids content of 957% and 9% respectively was
219 obtained for the composite samples (over the entire depth of black sediment in a given core). These values
220 are statistically similar to the average water / solids content of discrete samples, suggesting that composite
221 sampling can be an acceptable method of identifying the properties of discrete samples for this site. This
222 result is important for sediment volume estimates, as composite samples can yield higher volumes and are
223 more readily gathered when compared to discrete samples; as a result composite samples were used for
224 other dewatering studies by the authors (e.g. Alimohammadi et al. 2019). The locations from which the
225 gravity core samples were taken were thought to effectively represent the entire basin. Average percent
226 water content (corresponding solids contents are shown in brackets) were measured for Areas A, B, C, and
227 D respectively, as follows: 1052%(11.5%), 1150%(10.3%), 1188%(8.9%), and 1153%(11.9%). Statistical
228 analysis of this data showed no significant difference between discrete, composite or area samples. These
229 results suggest that all black sediment samples are consistent in terms of water / solids content despite the
230 location from which they were taken. It can be concluded that this sediment maintained spatial consistency
231 throughout the BHSL (spatial direction), and therefore sediment gathered through composite sampling
232 should be representative of the average found throughout the basin.

233

234 The solids contents obtained from Area A and B (sampling locations are shown in Figure 1) using the
235 vacuum sampling technique were 0.5% and 2.8%, respectively. The solids content of vacuum samples was
236 significantly lower than that obtained by gravity coring (discrete and composite), because of water mixing
237 with the sediments during the procedure (Figure 5(b)). Even though the same sampling procedure was
238 used for both Areas A and B, a lower water content and a higher solids content was measured in Area B,
239 which can be explained by the fact that thickness of black sediment is greater at the location of sampling in
240 Area B, allowing the intake to be more immersed in the sediment at the time of sampling. This confirms that
241 water / solids content measurements are not comparable to gravity core methods due to the high level of
242 disturbance in the samples.

243

244 Particle size distributions of discrete sample BH 19-01 and vacuum sample BHVP 18-01 (taken from
245 Area B), two composite samples BH17-57, BH17-58, and vacuum sample of BHVP 18-05 (taken from Area
246 A) are presented in Figure 6(a). Results show that the black sediment had a similar particle size distribution
247 at various depths and locations, regardless of the sampling method. The results (Figure 6(a)) indicate that
248 85% of sediment particles (discrete or composite) are finer than 11 μm ($D_{85} = 11 \mu\text{m}$). However, a D_{85} value
249 of vacuum sampling was slightly less than 11 μm as shown in this figure, indicating that sediment particles
250 obtained by vacuum sampling were slightly finer compared to coring samples. The majority (>80%) of
251 particles ($\sim 10^7$) range between 2 μm -10 μm , in the case of gravity coring (Figure 6(b)). As the particle size
252 increased from 10 μm to 100 μm , the number of particles decreased from $\sim 10^6$ to $\sim 2 \times 10^3$. When obtained
253 by vacuum sampling, however, the black sediment contains fewer particles at each certain size compared
254 to sampling by gravity coring. For instance, the number of particles at 100 μm and 200 μm is 100 and 10,
255 respectively, in BHVP samples, while results show almost 20 times more in coring samples (discrete and
256 composite). These findings show that sediment / water mixing during the vacuum sampling results in
257 dilution (a decrease in the number of particles), and perhaps a reduction in aggregation of particles during
258 the process.

259
260 Geotextile dewatering is one feasible option for recovering and processing these sediments prior to
261 containment based on studies related to developing remediation options for the BHSL (GHD, 2018). An
262 understanding of particle size becomes important as it influences dewatering. Figure 7 compares the range
263 of average (mean) size of the black sediment particles at different depths to that of the composite and
264 vacuum samples. The average particles size ranged between approximately 6 μm and 12 μm . One-way
265 ANOVA test (Tukey method) results indicate that there was no significant difference in particle size at
266 various depths. Tukey's results are shown with the letters on the graph 7, and samples attributed with
267 identical letters are not significantly different.

268 In addition, the average particle size of composite samples was statistically similar to discrete samples at
269 various depths, and at different locations in the BHSL (9.3 μm , 10.0 μm , 10.4 μm , and 10.5 μm for Area A,
270 B, C, and D respectively). The vacuum sampling method resulted in similar particle sizes distribution

271 (slightly larger for Area A (9.9 μm) and finer for Area B (8.9 μm)) to other composite and discrete samples,
272 indicating that sediments throughout the BHSL are consistent in terms of particle size.

273

274 **4. Conclusions**

275 This paper presents results of a field sampling program performed to assess the impact of various sampling
276 methods (i.e. discrete versus composite versus vacuum) on the physical characteristics of contaminated
277 sediments obtained from a large effluent stabilization lagoon. The overall objective of this paper was to use
278 this “field lab” as the basis for assessing how different sampling techniques can be relied upon for
279 representative samples for remediation-based evaluations (i.e. sediment volume estimates and bench scale
280 dewatering studies). A method of comparing time-consuming discrete sampling techniques to more time-
281 efficient composite sample techniques was presented as well as a method of comparing composite
282 sampling techniques to a vacuum sampling technique developed for this project.

283

284 The distribution of sediment thickness measured throughout the lagoon by gravity core sampling was
285 shown to vary substantially throughout the 160 ha site. Extrusions of these gravity core samples to obtain
286 discrete and composite samples indicate that there was no significant difference between physical
287 characteristics (water / solids content, density, particle size) of composite samples taken from different
288 areas within the BHSL when compared to discrete samples. For this particular site, it appears that
289 composite sampling would provide reasonable physical parameters when compared to more time-
290 consuming discrete sampling methods (i.e. should reflect the overall physical characteristics of the black
291 sediment throughout the basin for practical purposes).

292

293 The physical characteristics of vacuum-obtained samples were compared to gravity core samples (both
294 discrete and composite). This sampling method resulted in more water entrained in the samples, lower
295 solids content (~0.5–2.8%) and slightly finer particles in the samples. However, the mean particle size for
296 the vacuum sampling was not statistically different than that of discrete and composite samples.

297

298 The sampling evaluation process investigated in this study provides evidence that more expeditious
299 methods can be used to characterize sediments over large-scale, both in spatial and stratigraphic extent.
300 The results may also provide guidance on how to choose sampling techniques for obtaining representative
301 samples for aquatic sediment projects. .

302

303

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309

310 **References**

- 311 Alimohammadi M, Tackley H, Lake CB et al. (2019): Effect of different sediment dewatering techniques on
312 subsequent particle sizes in industrial derived effluent. *Canadian Journal of Civil Engineering*.
313 10.1139/cjce-2019-0269.
- 314 ASTM (2014) D 2974-14: Standard Test Methods for Moisture, Ash, and Organic Matter of Peat and Other
315 Organic Soils. ASTM International, West Conshohocken, PA, USA.
- 316 ASTM (2019) D 2216-19: Standard Test Methods for Laboratory Determination of Water (Moisture) Content
317 of Soil and Rock by Mass. ASTM International, West Conshohocken, PA, USA.
- 318 ASTM (2014) D 854 – 14: Standard Test Methods for Specific Gravity of Soil Solids by Water Pycnometer.
319 ASTM International, West Conshohocken, PA, USA.
- 320 Dunnington DW, White H, Spooner IS et al. (2017): A paleolimnological archive of metal sequestration and
321 release in the Cumberland Basin Marshes, Atlantic Canada. *J FACETS*, doi:10.1139/facets-2017-0004
- 322 Esri (2019). How Topo to Raster Works. See [https://pro.arcgis.com/en/pro-app/tool-reference/3d-](https://pro.arcgis.com/en/pro-app/tool-reference/3d-analyst/how-topo-to-raster-works.htm)
323 [analyst/how-topo-to-raster-works.htm](https://pro.arcgis.com/en/pro-app/tool-reference/3d-analyst/how-topo-to-raster-works.htm)
- 324 GHD Limited (2018) Phase 2 Environmental Site Assessment, Boat Harbour Remediation Planning and
325 Design, Pictou County, Nova Scotia, Nova Scotia Land Inc., Project No. 11148275, Report No. 6.
- 326 Glew JR, Smol JP and Last WM (eds) (2001) Tracking Environmental Change Using Lake Sediments. In
327 *Sediment Core Collection and Extrusion*. Springer, Dordrecht, vol. 1: Basin Analysis, Coring, and
328 Chronological Techniques, pp. 73–105, <https://doi.org/10.1007/0-306-47669-X>
- 329 Hoffman E, Lyons J, Boxall J et al. (2017) Spatiotemporal assessment (quarter century) of pulp mill
330 metal(loid) contaminated sediment to inform remediation decisions. *Environmental Monitoring and*
331 *Assessment* **189(6)**: 257-274. doi: 10.1007/s10661-017-5952-0.
- 332 Hoffman E, Alimonhammadi M, Lyons J et al. (2019) Characterization and spatial distribution of organic
333 contaminated sediment derived from historical industrial effluents. *Environmental Monitoring and*
334 *Assessment* **191(9)**: 590. doi: 10.1007/s10661-019-7763-y.
- 335 Mackie AL (2010) Feasibility study of using cement kiln dust as a chemical conditioner in the treatment of
336 acid mine effluent. M.Sc. thesis, Department of Civil and Resource Engineering, Dalhousie University,
337 Halifax, Canada.

338 Mao S (1997) High water content sludge dewatering via freeze-thaw. Master thesis, Department of Civil
339 and Environmental Engineering, University of Alberta, Edmonton, Canada.

340 Minitab (2019) See [https://support.minitab.com/en-us/minitab-express/1/help-and-how-to/modeling-](https://support.minitab.com/en-us/minitab-express/1/help-and-how-to/modeling-statistics/anova/how-to/one-way-anova/before-you-start/overview/)
341 [statistics/anova/how-to/one-way-anova/before-you-start/overview/](https://support.minitab.com/en-us/minitab-express/1/help-and-how-to/modeling-statistics/anova/how-to/one-way-anova/before-you-start/overview/)

342 Reis E, Lodolo A, Miertus S (2007) Survey of sediment remediation technologies. International center for
343 science and high technology. See [https://clu-in.org/download/contaminantfocus/sediments/Survey-of-](https://clu-in.org/download/contaminantfocus/sediments/Survey-of-sediment-remediation-tech.pdf)
344 [sediment-remediation-tech.pdf](https://clu-in.org/download/contaminantfocus/sediments/Survey-of-sediment-remediation-tech.pdf)

345 Sharma DK, King D, Oma P, Merchant C (2010) Micro-Flow Imaging: Flow microscopy applied to sub-
346 visible particulate analysis in protein formulations. *AAPS Journal* **12(3)**: 455-464. doi: 10.1208/s12248-
347 010-9205-1

348 Spooner I, Dunnington D (2016) Boat Harbour gravity core sediment survey. Nova Scotia Lands Inc., Nova
349 Scotia, Canada,

350 Tackley H (2019) The behavior and migratory fate of select heavy metals during the dewatering of an
351 effluent derived sediment. Master thesis, Department of Civil and Resource Engineering Dalhousie
352 University, Halifax, Canada. Available from <http://hdl.handle.net/10222/76263>.

353 Williamson DF, Parker RA, Kendrick JS (1989) The box plot: a simple visual method to interpret data. *Ann*
354 *Intern Med* **110(11)**: 916-921. doi: <https://doi.org/10.7326/0003-4819-110-11-916>

355 Ya J (2017) Electro-dewatering Treatment of Pulp and Paper Mill Biosludge: The Effects of Conditioners.
356 Master thesis, Department of Chemical Engineering and Applied Chemistry University of Toronto,
357 Canada.

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360 **Figure Captions**

361 Figure 1. Spatial coverage of sediment sampling locations in Boat Harbour (“BH 19” symbols identify
362 multiple samples taken within a 1 m distance from each other at a specific location).

363 Figure 2. Histogram of black sediment thickness for 151 gravity cores.

364 Figure 3. Isopach map of black sediment thickness based on 151 samples presented in this study.

365 Figure 4. (a) Water and (b) Solid contents at various depths taken via discrete sampling of selected cores
366 (dashed grey line shows interface between black and grey sediments, distances expressed from this
367 interface). The symbols represent the mean values, the error bars represent one standard deviation from
368 the mean.

369 Figure 5. (a) Water and (b) solids content variation of black sediment in discrete and bulk samples.

370 Samples labelled with identical letters (i.e. a, b, or c,) were not significantly different from each other (p
371 <0.05 level). Samples labelled with different letters are significantly different from each other ($p < 0.05$ level).

372 Vertical lines denote areas from which samples were obtained (i.e. Area A, B, C or D).

373 Figure 6. (a) Particle size, and (b) count distribution of discrete samples of (BH 19-01), composite core
374 samples of (BH17-57 and BH17-58), and Vacuum samples of (BHVP 18-01 and BHVP 18-05)

375 Figure 7. Variation in mean particle size versus depth and location. Samples labelled with identical letters
376 (i.e. a) were not significantly different from each other ($p < 0.05$ level).